

# Oxygen permeability of silicon-containing network polyamide and copolyamide films

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Network polyamide films (EY) of trimesic acid (Y) and 1,3-bis(3-aminopropyl)tetramethyldisiloxane (E), and network copolyamide films (EY/En) of Y and E with aliphatic dicarboxylic acids (*n*) and those (EY/EE') of Y and E with 1,3-bis(3-carboxypropyl)tetramethyldisiloxane (E') were prepared. The prepolymer was prepared using a melt polycondensation method, and then a dimethylformamide solution of the prepolymer was cast on an aluminium plate. The cast film obtained was post-polymerized to form a network structure. Post-polymerized films were flexible, transparent and insoluble in common solvents. The molecular and supramolecular structures of these network polymers were characterized by infra-red absorption spectra, X-ray diffraction analysis, differential thermal analysis and thermomechanical analysis. Oxygen and nitrogen permeabilities increased with increasing temperature. EY homopolymer had  $P_{O_2}$  of  $4.6 \times 10^{-10}$  cm<sup>3</sup>(s.t.p.) cm cm<sup>-2</sup> s<sup>-1</sup> cmHg<sup>-1</sup> and  $P_{O_2}/P_{N_2}$  of 3.4 at 60°C. Incorporation of copolymer components En and EE' enhanced the oxygen and nitrogen permeabilities while decreasing the glass transition temperature ( $T_g$ ). The decrease of  $T_g$  increased  $P_{O_2}$ , which may be explained by enhancement of the flexibility of the molecular chain. For the EY/EE' copolymer, an increase in the EE' component gave rise to an increase of  $P_{O_2}$  and a smaller decrease of  $P_{O_2}/P_{N_2}$ . The EY/EE'(10/90 mol%) film had the highest value of  $P_{O_2}$  of  $3.2 \times 10^{-9}$  cm<sup>3</sup>(s.t.p.) cm cm<sup>-2</sup> s<sup>-1</sup> cmHg<sup>-1</sup> and  $P_{O_2}/P_{N_2}$  of 2.8 at 60°C.

(Keywords: oxygen permeability; silicon-containing network film; siloxane moiety; glass transition temperature; flexibility of molecular chain; polyamides)

## INTRODUCTION

Silicon-containing polyamides<sup>1-7</sup> have been investigated for the purpose of improving processability, thermo-oxidative stability and mechanical properties. The oxygen permeability of silicon-containing polymers has been extensively investigated for the application of these materials to fuel combustion systems and in purification of air for medical purposes<sup>8</sup>. We have synthesized polyamides<sup>9</sup>, copolyamides<sup>10</sup> and polyimides<sup>11</sup> with siloxane moieties in their main chains, and polyamides and polyesters with siloxane moieties in their side-chains<sup>12</sup>, and have characterized their properties and oxygen permeability. Furthermore, we have synthesized novel network polyesters<sup>13-15</sup> and polyamides<sup>16</sup>, and have investigated their high resistance to heat distortion. Recently, we synthesized novel network polyamides and copolyamides with siloxane moieties in their main chains.

In this study, we report on a method of preparation of these novel network polyamides and copolyamides with siloxane moieties in their main chains, and discuss the molecular structure, thermal properties as well as oxygen permeability of these network polymers.

## EXPERIMENTAL

### Monomers

Figure 1 shows the structural formulae and codes of the tricarboxylic and dicarboxylic acids and diamine monomers. Trimesic acid triethyl ester was obtained by refluxing trimesic acid (Y) in ethanol at 80°C for 4 h in the presence of H<sub>2</sub>SO<sub>4</sub> as a catalyst. The trimesic acid triethyl ester obtained was recrystallized from ethanol

solution and then dried at 50°C for 24 h *in vacuo*. 1,3-Bis(3-aminopropyl)tetramethyldisiloxane (E) and 1,3-bis(3-carboxypropyl)tetramethyldisiloxane (E'), donated by Chisso Corp., Japan, were used without further purification. Malonic acid diethyl ester (3), adipic acid (6), azelaic acid (9) and 1,10-decanedicarboxylic acid (12) were used as received.

### Preparation of prepolymers

A mixture of trimesic acid triethyl ester and E, in which aliphatic dicarboxylic acid was added for copolymerization, was heated up from room temperature to 140°C for 1-1.5 h, and further heated to 190-220°C at the rate of 0.5°C min<sup>-1</sup>.

### Film preparation

The obtained prepolymer was cast on an aluminium plate from 12 wt% dimethylformamide (DMF) solution at 80-100°C.

### Post-polymerization of films

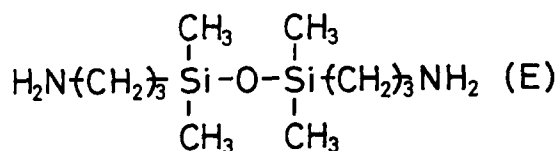
The cast film was post-polymerized under a stream of nitrogen in an electric furnace. After the aluminium substrate was dissolved off in a 10 wt% sodium hydroxide solution, a transparent and flexible film was obtained.

### Characterization

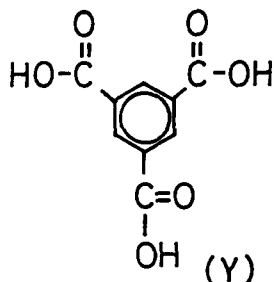
The molecular-weight distribution of the prepolymer was determined by a Toyo Soda HLC-802A gel permeation chromatograph with TSK gel G2000H column standardized by polystyrene.

Thermomechanical analysis (t.m.a.) was performed in

Diamine monomer



Triacid monomer



Diacid monomers

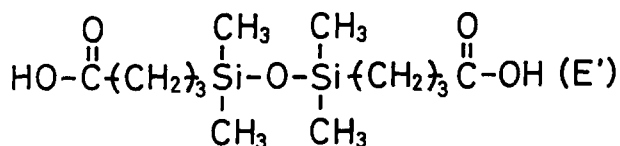
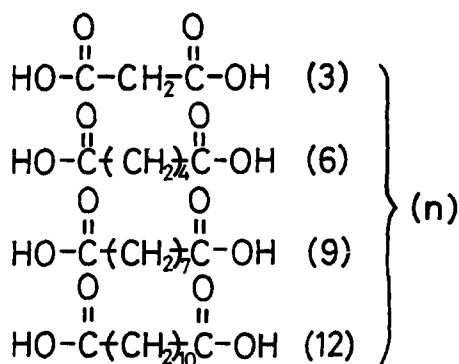


Figure 1 Structural formulae and codes of chemicals used in this study

the penetration mode under 10 kg cm<sup>-2</sup> pressure at a heating rate of 10°C min<sup>-1</sup> in nitrogen atmosphere, using a Shimadzu model DT-30 thermomechanical analyser.

Infra-red spectra were recorded on a Jasco model IR A-1 spectrophotometer using a KBr pellet or a thin film.

X-ray diffraction intensity was measured with a Toshiba model ADG-301 X-ray diffractometer with nickel-filtered Cu K $\alpha$  radiation.

Differential thermal analysis (d.t.a.) was carried out on a Shimadzu model DT-30 differential thermal analyser at a heating rate of 10°C min<sup>-1</sup> in nitrogen atmosphere.

Thermogravimetry (t.g.) was performed on a Shimadzu model DT-30 thermogravimetric analyser at a heating rate of 10°C min<sup>-1</sup> in nitrogen atmosphere.

Gas permeability

Gas permeability was measured by Rikaseiki model K-315-N equipped with an MKS Baratron pressure transducer. The volume of gas permeating through a polymer film from upstream (including the permeation gas) to downstream in a vacuum of 0.1 mmHg was measured by the pressure transducer. The permeability coefficient *P* was calculated by the equation:

$$P = \frac{dp}{dt} \frac{L}{A} \frac{T_0}{p_0} \frac{1}{p} \frac{V}{T}$$

where *dp/dt* is the slope at steady state in the permeation curves, *L* is film thickness, *A* is film area, *T*<sub>0</sub> and *p*<sub>0</sub> are the temperature and pressure under standard conditions, *p* is the pressure of supplied gas, *V* is the cell volume downstream (including the pressure transducer) and *T* is the temperature of cell.

RESULTS AND DISCUSSION

Homopolymer film

Conditions of synthesis. Figure 2 shows the g.p.c. curve of EY prepolymer prepared by heating to 220°C at a rate of 0.5°C min<sup>-1</sup>. Table 1 illustrates the molecular structures

Table 1 Molecular structures of EY prepolymers estimated from the observed molecular weight; numbers 1-5 correspond to those in Figure 2

| No. | Structure <sup>a</sup>             | Molecular weight |      |
|-----|------------------------------------|------------------|------|
|     |                                    | Calc.            | Obs. |
| 1   | H <sub>2</sub> N-R-NH <sub>2</sub> | 248              | 150  |
| 2   |                                    | 294              | 312  |
| 3   |                                    | 496              | 459  |
| 4   |                                    | 698              | 672  |
| 5   |                                    | 1526             | 1532 |

<sup>a</sup> R =  $\text{-(CH}_2\text{)}_3\text{Si}(\text{CH}_3)_2\text{O}(\text{CH}_2\text{)}_3\text{Si}(\text{CH}_3)_2\text{-}$

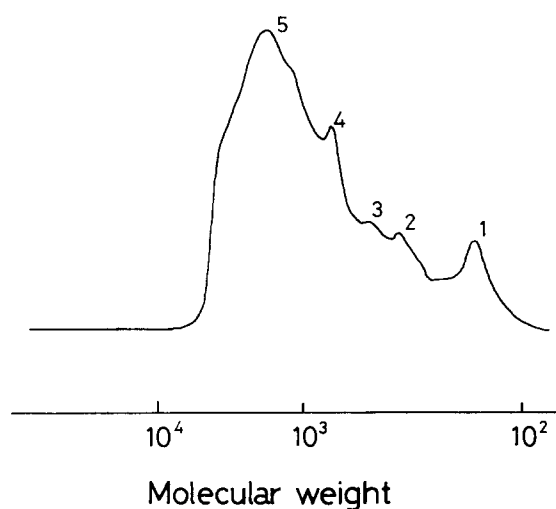


Figure 2 G.p.c. curve of EY prepolymer

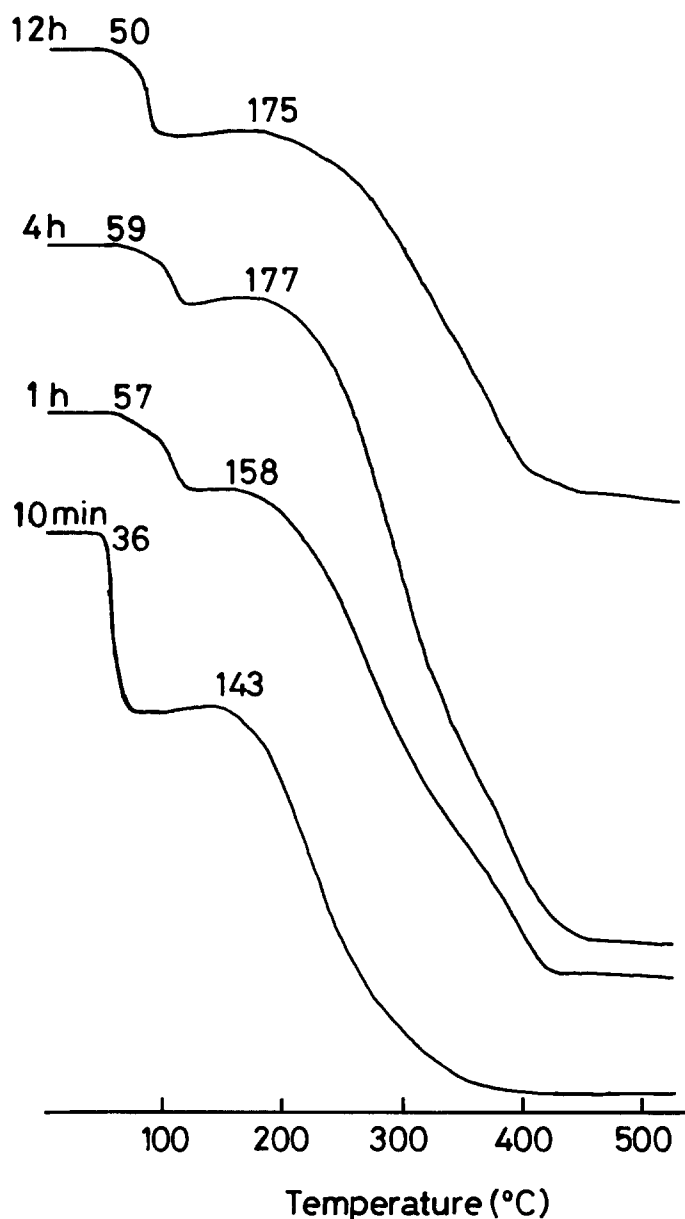


Figure 3 T.m.a. curves of EY post-polymerized for various times at 280°C

of prepolymer estimated from the observed molecular weights of peaks 1–5 in Figure 2. The estimated molecular structure in Table 1 shows that the polymerization progresses stepwise and the molecular chain extends to two or three dimensions.

After casting the obtained prepolymer, it was post-polymerized to form a network. Figure 3 shows the t.m.a. curves of EY post-polymerized for various times at 280°C, in which the t.m.a. probe penetrates into the polymer film stepwise. The inflection point of the t.m.a. curve, the heat distortion temperature, increases with increasing post-polymerization time. The dependence of the distortion temperature on the post-polymerization time at temperatures of 240, 280 and 300°C is shown in Figure 4. The first and second distortion temperatures increase with increasing post-polymerization time and level out above a post-polymerization time of 4 h. A film post-polymerized at higher temperature has a higher second distortion temperature, but there is no significant difference between the first distortion temperatures among three films post-polymerized at various temperatures. The second distortion temperature of EY corresponds to the heat distortion temperature of 187°C for 9Y having the same number of bonds per repeat unit in the main chain<sup>16</sup>. A film post-polymerized at 300°C considerably coloured, probably because of partial thermal decomposition at high temperature. Therefore the post-polymerization temperature and time were set as 280°C and 4 h. All post-polymerized films were flexible and transparent and insoluble in common solvents.

*Structure and properties.* Infra-red absorptions due to Si–O stretching, C=O stretching (amide I) and

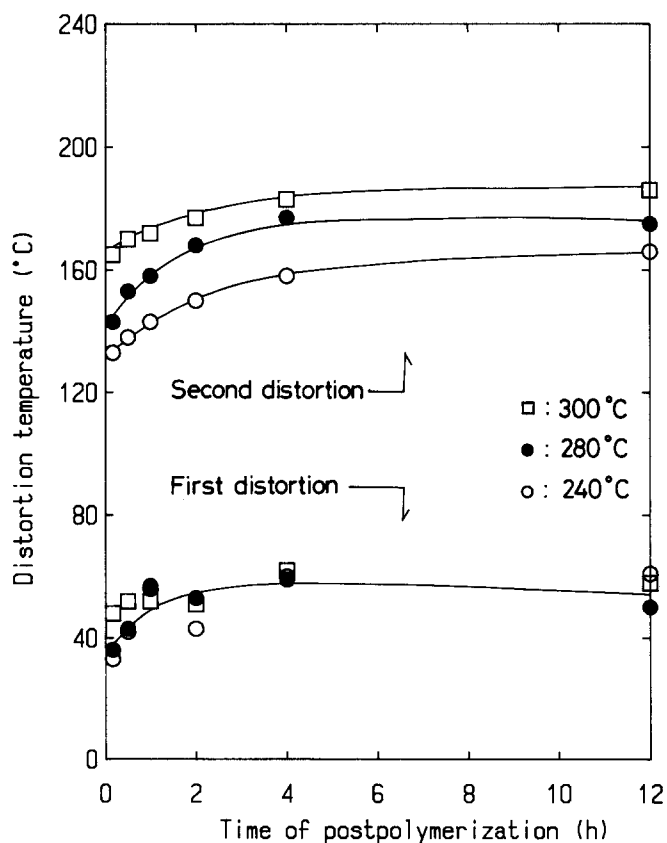


Figure 4 Plots of first and second distortion temperatures of EY against post-polymerization time

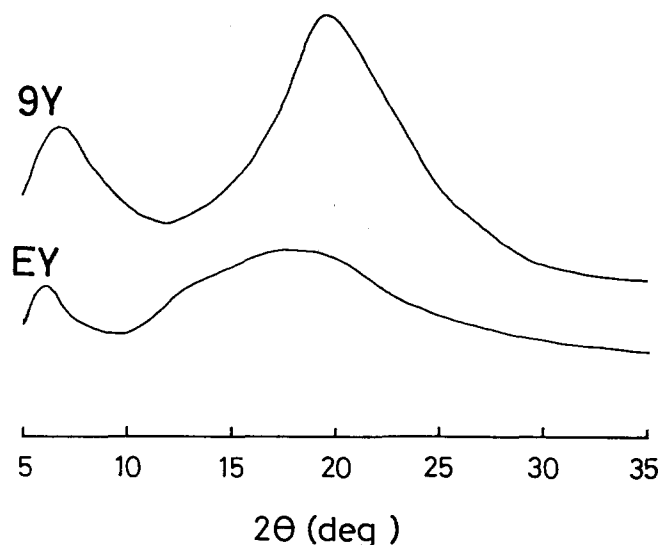


Figure 5 X-ray diffraction intensity curves of EY and 9Y

N-H bending (amide II) were confirmed at 1050, 1640 and 1540  $\text{cm}^{-1}$ , respectively. The absorption peak at 1720  $\text{cm}^{-1}$  due to C=O stretching of free carboxylic acid decreased with increasing post-polymerization time. The ratio between the absorbance at 1720  $\text{cm}^{-1}$  and that at 1640  $\text{cm}^{-1}$  decreased with post-polymerization time and almost levelled off above a post-polymerization time of 4 h, which corresponds well to the fact that the distortion temperature is almost levelled out above a post-polymerization time of 4 h as shown in Figure 4.

Figure 5 shows a comparison of X-ray diffraction curves of EY and 9Y. Both EY and 9Y have two broad but distinct peaks. The spacings for EY calculated using Bragg's equation are 14.7 and 4.9 Å, corresponding to the peaks of  $2\theta = 6^\circ$  and  $18^\circ$ , respectively. The diffraction around  $6^\circ$  may be ascribed to that from some ordered structure due to the alignment of the benzene ring in the direction of the main chain; and that around  $18^\circ$  is probably related to the intermolecular alignment of the benzene ring. The diffraction peak around  $18^\circ$  of EY is broader than that of 9Y, which implies that steric hindrance of the dimethyl side-group in component E may depress the formation of an ordered structure. D.t.a. showed two endothermic transitions at 46 and  $104^\circ\text{C}$  for EY. The lower transition temperature corresponds to the first distortion temperature measured by t.m.a. At the present stage, we do not have an exact answer for the appearance of two endothermic transitions, but we consider that the lower endothermic transition is the glass transition temperature. T.g. gave the temperature of 10% weight loss as  $414^\circ\text{C}$  and  $410^\circ\text{C}$  and the residue at  $600^\circ\text{C}$  of 18 and 16% for EY and 9Y, respectively, showing that the thermal stability of component E is comparable to that of the methylene chain.

**Gas permeability.** Figure 6 shows the temperature dependence of permeability coefficients of oxygen ( $P_{\text{O}_2}$ ) and nitrogen ( $P_{\text{N}_2}$ ). The notation  $T_i$  in this figure will be discussed later. The activation of the segmental motion with increasing temperature makes the free volume larger, and thus the permeation of oxygen and nitrogen is enhanced by increasing temperature. The values  $P_{\text{O}_2}$  of  $4.6 \times 10^{-10} \text{ cm}^3(\text{s.t.p.}) \text{ cm cm}^{-2} \text{ s}^{-1} \text{ cmHg}^{-1}$  and  $P_{\text{O}_2}/P_{\text{N}_2}$  of 3.4 were obtained at  $60^\circ\text{C}$ . We have reported that silicon-containing polyamide of E6 prepared from

E and adipic acid has  $P_{\text{O}_2}$  of  $20.4 \times 10^{-10} \text{ cm}^3(\text{s.t.p.}) \text{ cm cm}^{-2} \text{ s}^{-1} \text{ cmHg}^{-1}$  and  $P_{\text{O}_2}/P_{\text{N}_2}$  of 2.7 at  $60^\circ\text{C}$ . The Si content of E6 of 15.6 wt% is comparable to that of EY of 15.9%. Thus, the lower  $P_{\text{O}_2}$  value of EY is probably ascribed to the rigid Y molecule. Therefore, we tried to obtain more oxygen-permeable film through the incorporation of a flexible aliphatic chain by copolymerization, as studied below.

#### Copolymer films

**Structure and properties.** Figure 7 shows the X-ray diffraction curves of EY/En and EY/EE' with EY content of 50 mol% as well as EY homopolymer. The intensity around  $6^\circ$  decreases with the incorporation of aliphatic copolymer component owing to a decrease in the network.

D.t.a. curves are shown in Figures 8a for EY/En and 8b for EY/EE'. The observed endothermic transition corresponds to the glass transition of these copolymers. The glass transition temperature ( $T_g$ ) decreases on increasing the length of methylene chains in the aliphatic copolymer component, which is ascribed to the flexibility of aliphatic molecular chains. The increase of EE' component in EY/EE' also decreases  $T_g$ .

Table 2 shows the temperature of 10% weight loss and the residue at  $600^\circ\text{C}$  measured by t.g. Increase in the length of methylene chains in the aliphatic copolymer component leads to a decrease in the temperature of 10% weight loss, while the residue at  $600^\circ\text{C}$  is almost the same for all copolymers irrespective of the kind of aliphatic copolymer component.

**Gas permeability.** Figure 9 shows the temperature dependence of  $P_{\text{O}_2}$  and  $P_{\text{N}_2}$  for EY/E9(50/50 mol%) copolymer. No significant hysteresis of the permeability is observed during heating and cooling through the glass transition temperature. The slope of the Arrhenius plot

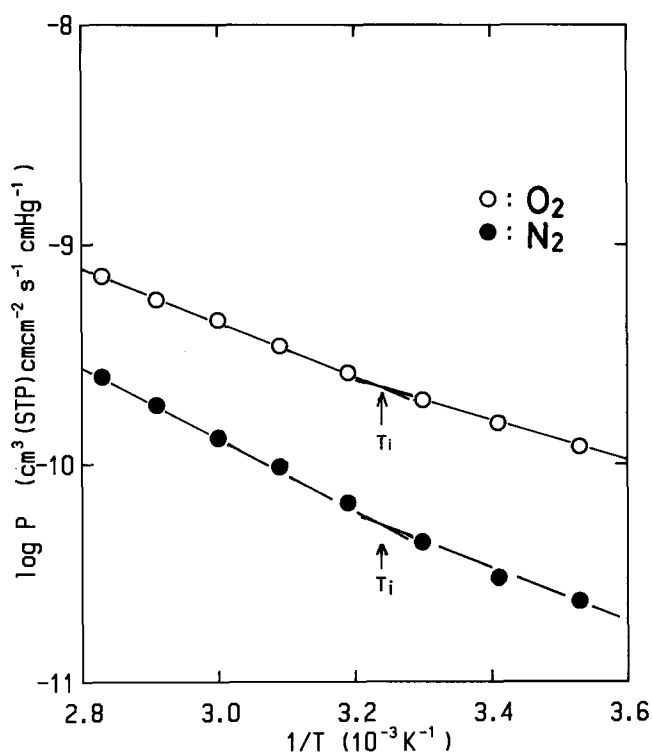


Figure 6 Temperature dependence of  $P_{\text{O}_2}$  and  $P_{\text{N}_2}$  for EY

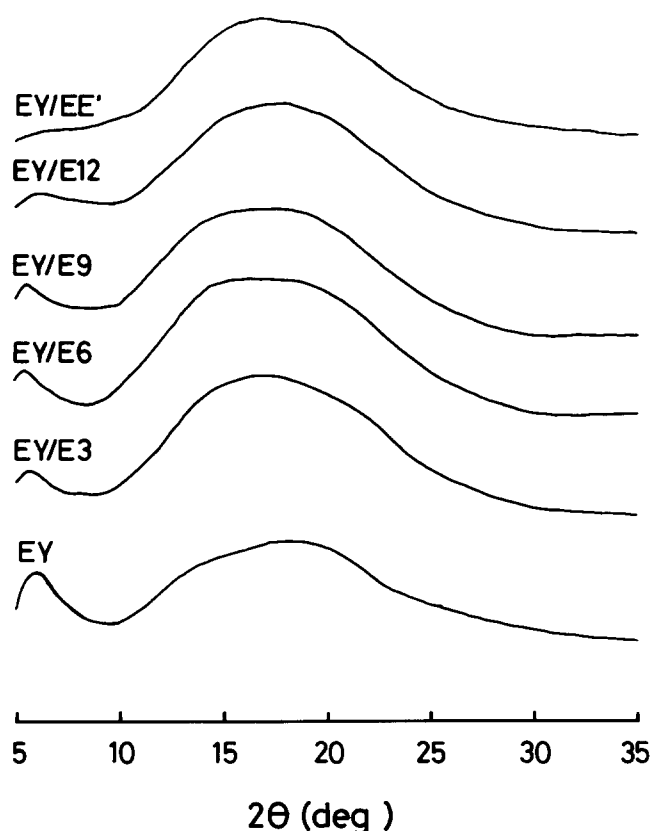


Figure 7 X-ray diffraction intensity curves of EY/En

of the permeability coefficient is different above and below  $T_i$ . Other polymer films of EY/E3, EY/E6, EY/E12, EY/EE' and EY also showed similar behaviour on the temperature dependence of the permeability coefficient. The  $T_i$  value is plotted against the glass transition temperature ( $T_g$ ) of each polymer in Figure 10. A linear relationship between  $T_i$  and  $T_g$  is obtained, although  $T_g$  is  $\sim 10^\circ\text{C}$  higher than  $T_i$ ;  $T_i$  is regarded as a transition temperature for gas permeability;  $T_g$  is the temperature at which micro-Brownian motion commences, and segmental mobility is largely enhanced above  $T_g$ , and thus the dependence of permeability on temperature might be changed.

Figure 11 shows the dependence on Si content of  $P_{\text{O}_2}$  of EY/En and EY/EE' as well as EY.  $P_{\text{O}_2}$  increases with decreasing Si content. This result suggests that silicon content is not the only factor affecting the higher permeation of oxygen in silicon-containing polymers. These permeabilities are replotted against the  $T_g$  of each polymer in Figure 12.  $P_{\text{O}_2}$  increases with decreasing  $T_g$ , which shows that the segmental mobility estimated by  $T_g$  dominates the permeation of oxygen. The longer methylene chains in the copolymer unit reduce  $T_g$  and therefore enhance  $P_{\text{O}_2}$ . In Figure 12, it is noted that EY/EE' has larger  $P_{\text{O}_2}$  in spite of higher  $T_g$ . Figure 13 shows the Si content dependence of  $P_{\text{O}_2}$  on changing the EE' content in EY/EE'. In this case,  $P_{\text{O}_2}$  increases with increasing Si content and with decreasing  $T_g$ . EY/EE'(10/90 mol%) had the highest value of  $P_{\text{O}_2}$  of  $3.2 \times 10^{-9} \text{ cm}^3(\text{s.t.p.}) \text{ cm cm}^{-2} \text{ s}^{-1} \text{ cmHg}^{-1}$  and  $P_{\text{O}_2}/P_{\text{N}_2}$  of 2.8 at  $60^\circ\text{C}$ .

The values of  $P_{\text{O}_2}$  are plotted against the separation factor for all samples in Figure 14. Increase of  $P_{\text{O}_2}$  gives a decrease of  $P_{\text{O}_2}/P_{\text{N}_2}$ . It is noted that the relation between  $P_{\text{O}_2}$  and  $P_{\text{O}_2}/P_{\text{N}_2}$  for EY/EE' is different from

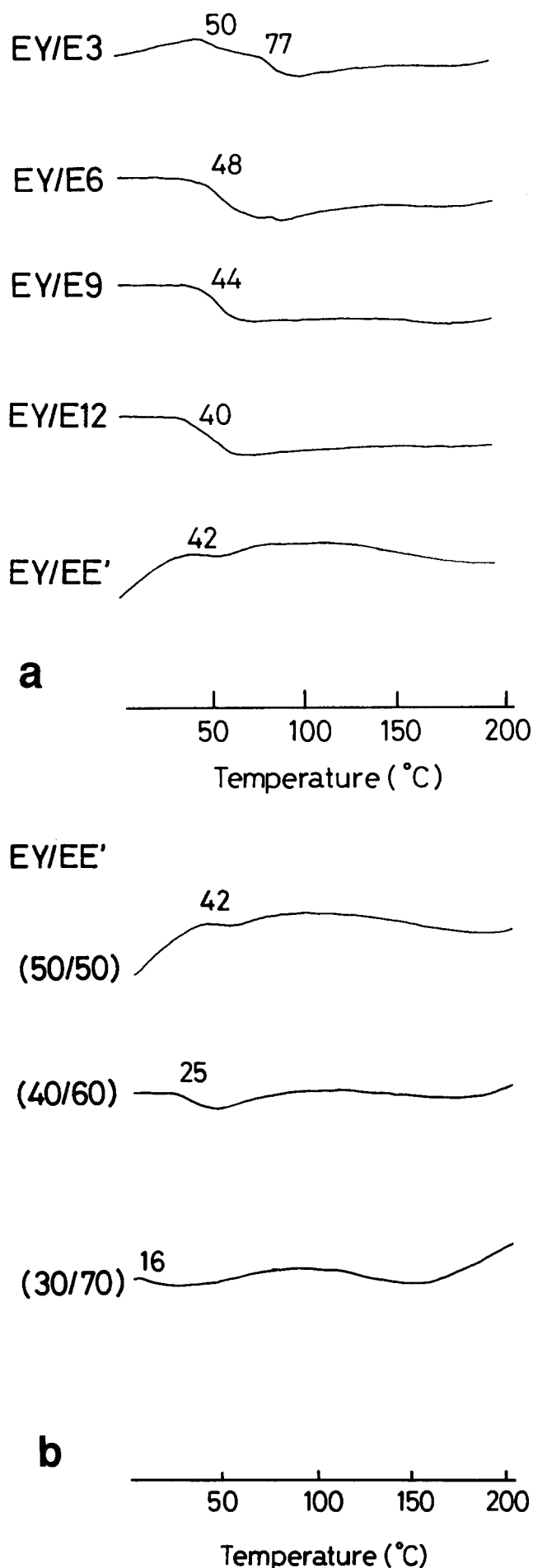
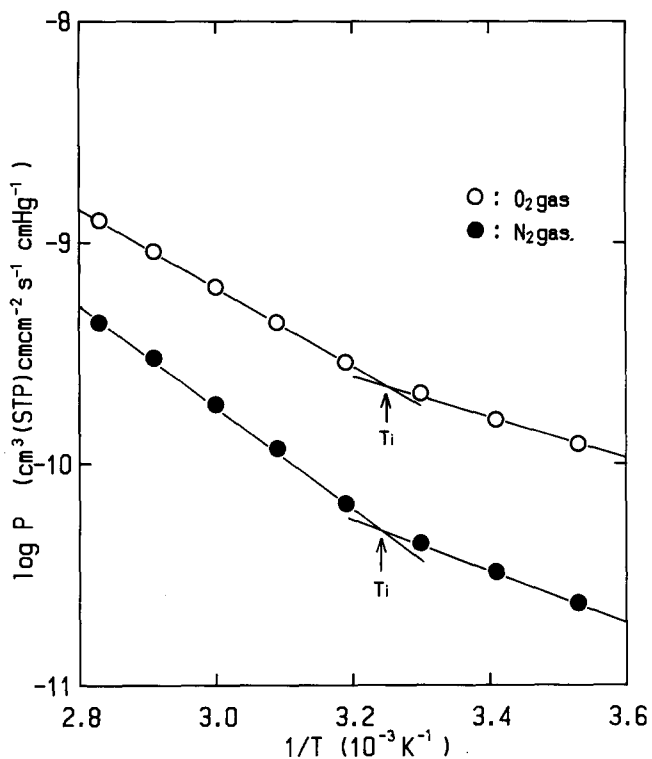


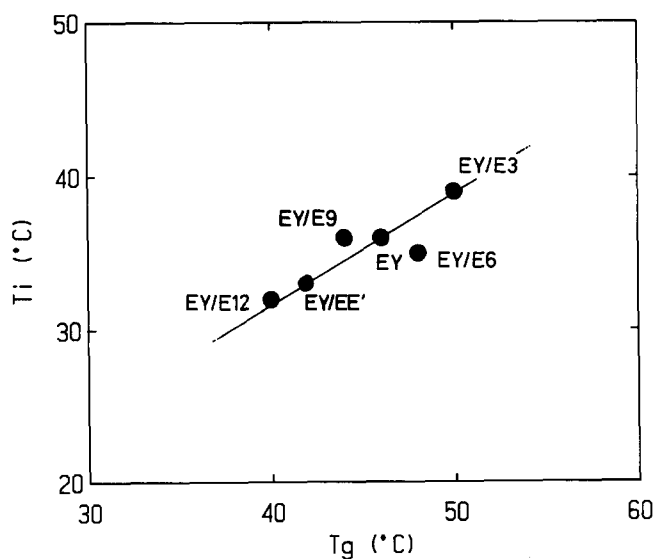
Figure 8 D.t.a. curves of (a) EY/En and (b) EY/EE'

**Table 2** Temperature of 10% weight loss and residue at 600°C for EY/En(50/50 mol%) and EY/EE'(50/50 mol%)

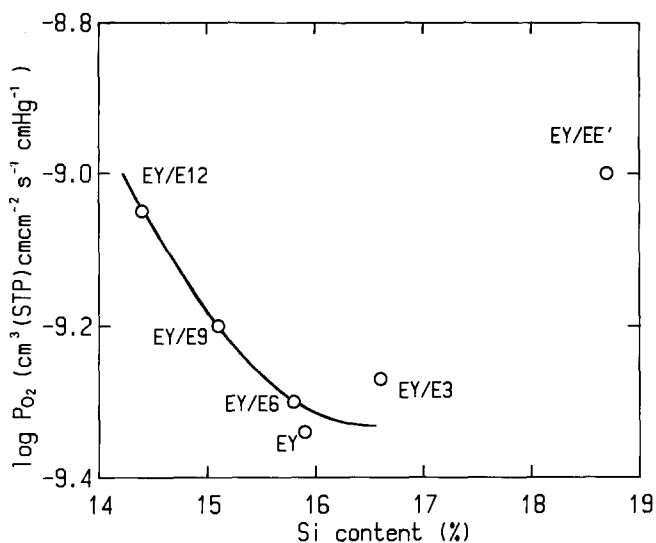
| Polymer | Temp. of 10% weight loss (°C) | Residue at 600°C (%) |
|---------|-------------------------------|----------------------|
| EY/E3   | 430                           | 16                   |
| EY/E6   | 399                           | 16                   |
| EY/E9   | 389                           | 16                   |
| EY/E12  | 379                           | 15                   |
| EY/EE'  | 372                           | 15                   |



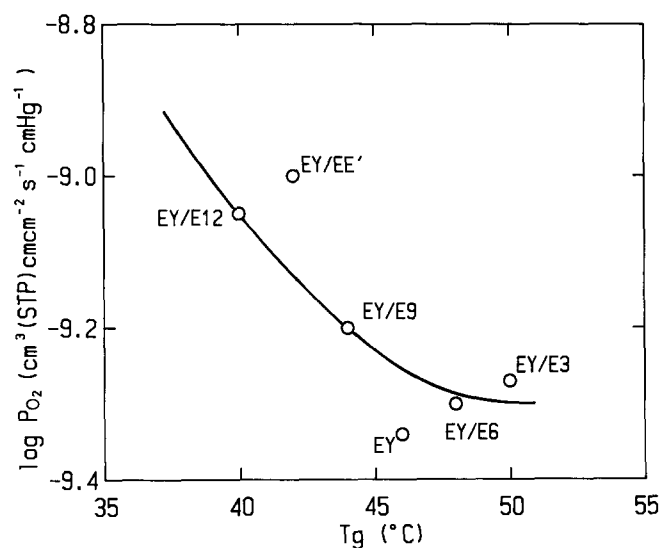
**Figure 9** Temperature dependence of oxygen and nitrogen permeabilities for EY/E9(50/50 mol%)



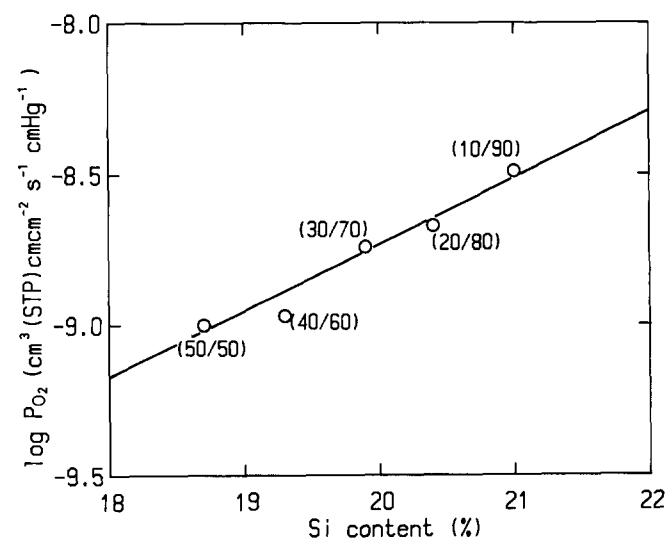
**Figure 10** Plots of  $T_i$  against  $T_g$  for EY, EY/En and EY/EE'. Content of EY component in copolymer is 50 mol%



**Figure 11** Si content dependence of  $P_{O_2}$  for EY, EY/En and EY/EE'. Content of EY component in copolymer is 50 mol%



**Figure 12** Plots of  $P_{O_2}$  against  $T_g$  for EY, EY/En and EY/EE'. Content of EY component in copolymer is 50 mol%



**Figure 13** Si content dependence of  $P_{O_2}$  for EY/EE'

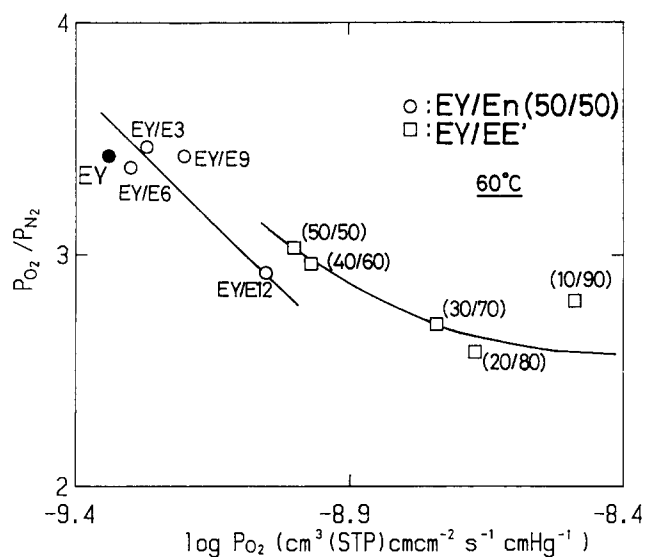


Figure 14 Plots of  $P_{O_2}/P_{N_2}$  against  $P_{O_2}$  for all network films studied

that for EY/En. In other words, EY/EE' has higher  $P_{O_2}/P_{N_2}$  compared with the extrapolated value from EY/En. This result implies that the increase of EE' component, the increase of siloxane moiety, causes a higher oxygen permeability with a smaller decrease of separation factor.

## CONCLUSIONS

Oxygen and nitrogen permeabilities of silicon-containing network polymer films of EY, EY/En and EY/EE' have been investigated.

These network polymer films were prepared through soluble prepolymers and subsequent post-polymerization of cast prepolymer films. Post-polymerized films were flexible, transparent and insoluble in common solvents.

Oxygen and nitrogen permeabilities increased with increasing temperature. EY homopolymer had  $P_{O_2}$  of  $4.6 \times 10^{-10}$  cm<sup>3</sup>(s.t.p.)cm cm<sup>-2</sup>s<sup>-1</sup>cmHg<sup>-1</sup> and  $P_{O_2}/P_{N_2}$  of 3.4 at 60°C. The slope of the Arrhenius plot of permeability coefficient changed at a certain temperature  $T_i$ , which corresponds well to  $T_g$  of these network polymers. Incorporation of copolymer component of En and EE' enhanced the oxygen and nitrogen permeabilities with decreasing  $T_g$ . The decrease of  $T_g$  increased  $P_{O_2}$ , which may be explained by enhancement of the flexibility

of the molecular chain. For EY/EE', increase of E' component gave rise to an increase of  $P_{O_2}$  with a smaller decrease of  $P_{O_2}/P_{N_2}$ . EY/EE'(10/90 mol%) film had the highest value of  $P_{O_2}$  of  $3.2 \times 10^{-9}$  cm<sup>3</sup>(s.t.p.)cm cm<sup>-2</sup>s<sup>-1</sup>cmHg<sup>-1</sup> and  $P_{O_2}/P_{N_2}$  of 2.8 at 60°C. It is noted that the introduction of network structure by copolymerization of Y with EE' polymer enables a film to be formed, although EE' homopolymer has less processability to make a film.

## ACKNOWLEDGEMENTS

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